

Testing of a Bipolar Solid-State Marx Generator for Berlin BESSY II Injection Kicker System

L. M. Redondo¹, Senior Member, IEEE, A. Kandratsyev, T. Atkinson, and O. Dressler

Abstract—This article describes the preliminary results from the new bipolar solid-state Marx generator proposed for Berlin BESSY II injection system, which includes the following pulse specifications: (1) peak voltage of ± 8 kV, (2) peak current of 160 A, (3) impedance of 50 Ω , (4) frequency ≤ 10 Hz, (5) width of 350 ns, (6) risetime ≤ 80 ns, and (7) deviation from “Flat top” $\leq \pm 1\%$. The generator is based on SiC metal-oxide-semiconductor field-effect transistors (MOSFETs) in order to allow fast risetime/falltime, where the charging of the main capacitors is from resistive paths. A generator with ten stages, using a dummy load that simulates a kicker magnet, is experimentally tested in order to study the overall performance, and results are presented and discussed.

Index Terms—High-speed electronics, particle accelerator magnets, power metal-oxide-semiconductor field-effect transistors (MOSFETs), pulse power systems, solid-state Marx generator, Thyatron replacement.

I. INTRODUCTION

HIGH-VOLTAGE pulsed generators, based on semiconductor switch technology, are being actively developed nowadays to replace established hard-tube-based generators, using Thyatron and pulse-forming networks/lines (PFNs/PFLs), in accelerator applications [1]–[5]. One of the most promising switch technologies is the silicon carbide (SiC) metal-oxide-semiconductor field-effect transistors (MOSFETs), where the high-speed commutation characteristics, together with low losses, make this type of devices very attractive. However, the still relatively low voltage and current capabilities of the semiconductors, in particular SiC MOSFETs, impose the use of stack techniques to achieve the needed voltage and current pulse amplitudes for accelerator applications; one technique that has been actively pursued is the Marx generator topology [6]–[8].

This article is related to testing a bipolar Marx generator topology developed for the Berlin BESSY II injection kicker system [9]–[11]. Traveling wave kicker magnets are applied for injection into and extraction from the BESSY II

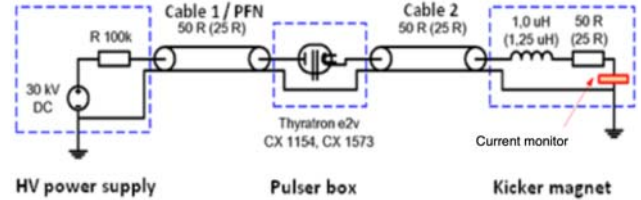


Fig. 1. Circuit topology of traveling wave kicker pulser systems for BESSY II booster.

booster synchrotron. The equipment is based on robust Thyatron switch technology and a rather simple circuit topology (Fig. 1). While the injection kicker system has a characteristic impedance of 50 Ω , the extraction kicker systems are designed for 25 Ω .

The characteristic of the circuit topology, in Fig. 1, is that the Thyatron is isolated from ground potential. A voltage pulse of half the PFN charging voltage is launched into cable 2 when the switch turns ON. This means that only half of the voltage is transferred to the load. For the duration of the pulse, the trigger electronics must withstand this half changing voltage as well [11].

The injection kicker magnet is energized over a 50- Ω cable from kicker pulser box. The HV supply, the kicker pulser box, and the trigger and control electronics are situated outside the booster tunnel with distance to the magnets. This fact makes a semiconductor-based generator replacement feasible, since semiconductors are more susceptible to higher failure rates when exposed to ionizing radiation, as it is the case if generator device is installed inside an accelerator tunnel. In addition, maintenance is easier outside the tunnel. A filter circuit could be introduced as well at the end of the cable for risetime shaping [11].

The not perfectly matched kicker magnet will cause a reflection between the magnet and the pulse generator. In order to delay this reflection for after the pulse, cable 2 has a length of 80 m.

The traveling wave kicker systems, as key components of the booster synchrotron, have a direct impact on the stable and uninterrupted top up mode operation of BESSY II synchrotron and storage ring. For the operation of BESSY II booster, the following is desired: (1) high availability and reliability of kicker systems during operation, (2) high average lifetime of the switches used, (3) best possible stability for suppressing timing jitter and drift, (4) high amplitude accuracy and simultaneously good flat-top of the current pulses, (5) small EMI, low sensitivity to external EMI radiation, and (6) steep falltime and risetime for turn OFF (injection) or turn ON (extraction kicker).

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However, various problems were detected on the pulser systems currently used, such as (1) damage of the insulation in the kicker pulser boxes by heating of the Thyratrons, (2) aging of the Thyatron causes timing drifts, (3) beating between the stable 10 Hz of the booster powering white circuits and 50-Hz line frequency, (4) short life time of the Thyratrons in the applied circuit topology, assumingly damaged by sharp risetimes, and (5) for the top up mode operation, the primary sides of the devices are permanently on HV.

Hence, the foreseen solution for the discovered deficiencies could be the development of new pulser systems based on the advanced technology of solid-state switches. Solid-state Marx generators have become a mature technology nowadays, being a reliable solution in several industrial applications, including accelerator applications for Thyatron replacement.

The pulse specifications for injection kicker include: (1) voltage up to 8 kV, positive or negative, (2) peak current of 160 A, (3) loop load impedance of 50 Ω , (4) repetition rate ≤ 10 Hz, (5) width of 350 ns, (6) risetime ≤ 80 ns, and (7) deviation from “Flat top” $\leq \pm 1\%$. The positive pulse current is required to power the kicker magnet for beam injection into the booster synchrotron. Both the polarities, positive and negative, are necessary if the kicker pulser device is used to drive a separate diagnostic kicker magnet as an exciter for beam studies.

Considering various stacked stages of a Marx generator, using semiconductor switches, several challenges become obvious, in order to fulfil the required specifications such as the synchronization of the semiconductor triggering, the jitter, and the fast risetime.

The presented article is dedicated to the development of a MOSFET based bipolar Marx proposed for Berlin BESSY II injection system, using a dummy load that simulates the Kicker magnet, for various operating conditions, in order to study its overall performance.

II. BIPOLAR MARX GENERATOR TOPOLOGY

A. General Marx Bipolar Topology

The simplified topology of a general bipolar solid-state generator, with n stages, capable of delivering repetitive positive and/or negative high voltage output pulses to a load, R_0 , using MOSFETs as ON-OFF switches, is presented Fig. 2, where $i \in \{1, \dots, n\}$.

In this topology, the number of main capacitors $C_n + 1$ exceeds by one of the solid-state switch stages, n , where the first capacitor, C_1 , just contributes to the positive pulses and the last, $C_n + 1$, to the negative pulses, as described in detail elsewhere [12]. Also, each stage comprises diodes, D_{ai} and D_{bi} and four switches, S_{ai} , S_{bi} , S_{pi} , and S_{ni} .

In the circuit presented in Fig. 2, the operating modes are rather simple as the C_i capacitors are charged from the U_{dc} PS when switches S_{ai} and S_{bi} are ON. The positive pulse is applied when switch S_{pi} is ON, and the negative pulse is applied when switch S_{ni} is ON, resulting in an applied output voltage with an amplitude of approximately $v_0 = \pm nU_{dc}$, considering no losses. However, the consequence for this simplicity is that the S_{pi} and S_{ni} switches hold-off a

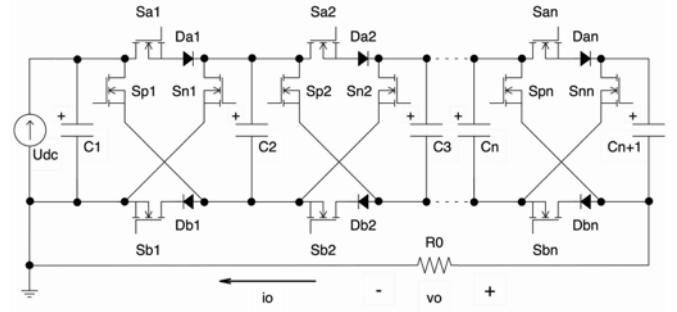


Fig. 2. General bipolar solid-state based Marx generator.

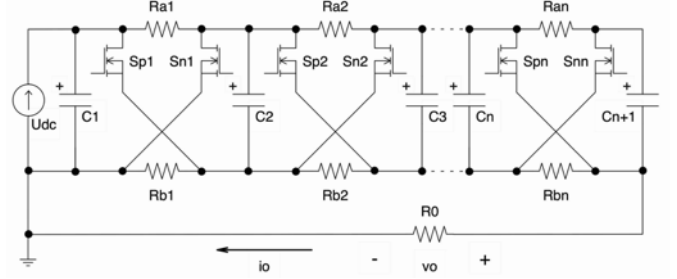


Fig. 3. Simplified bipolar solid-state based Marx generator.

voltage of $2U_{dc}$, respectively, during the negative and positive pulses [12].

B. Simplified Marx Bipolar Topology

The circuit in Fig. 2 can be simplified, replacing the charging switches S_{ai} and S_{bi} and diodes D_{ai} and D_{bi} , respectively, by resistors R_{ai} and R_{bi} , as shown in Fig. 3. This is possible as long as, during the charging mode, the capacitors C_i voltage rise up to U_{dc} , depending on: (1) the value of R , (2) the value of the operating frequency, and (3) the number of stages.

The three main operating modes of the circuit in Fig. 3 are presented in Fig. 4, where Fig. 4(a) is the charging mode, Fig. 4(b) is the positive pulse mode, and Fig. 4(c) is the negative pulse mode.

For the given circuit topology during the charging mode, in Fig. 4(a), the equation that describes the time to charge the n th stage with a dc source is given approximately by [2] as

$$T_{chg} = N^2 RC, \quad \text{where } 1 \leq n \leq N \quad (1)$$

where N is the stage number, $R = R_{bi} = R_{ai}$, and $C = C_i$. For this application, the time to charge the last capacitor to U_{dc} must be less than $1/(10 \text{ Hz}) = 100 \text{ ms}$. The design of these resistances must consider, also, the self-discharging current paths of the C_i capacitors, through these resistors, during the pulse modes [i.e., $i(R_{ai})$ and $i(R_{bi})$], as seen in Fig. 4(b) and (c). Where, considering $R = R_{bi} = R_{ai}$ and $v_{Ci} = U_{dc}$, these currents are approximately U_{dc}/R . Hence, during the pulse, each switch (i.e., S_{pi} and S_{ni}) must conduct a current given, as

$$i_0 = v_0/R_0 + 2U_{dc}/R. \quad (2)$$

Finally, for safety reason a switch was additionally placed in parallel with capacitor C_1 , so that in case of emergency, the Marx generator can be discharged rapidly (see Section III-B).

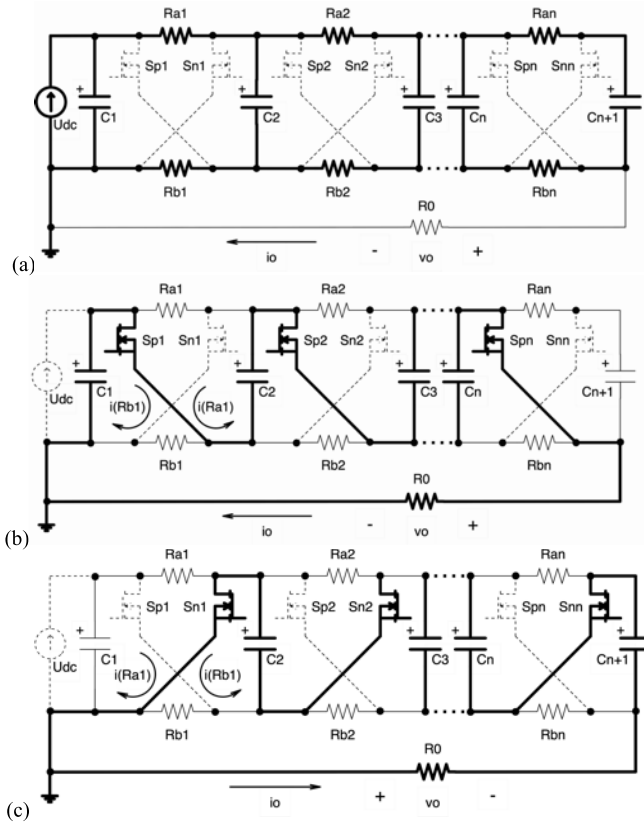


Fig. 4. Operating modes of Fig. 3 circuit. (a) Charging. (b) Positive pulse. (c) Negative pulse.

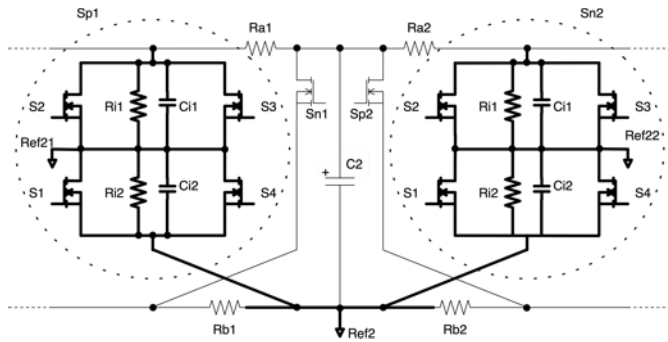


Fig. 5. Details of $Sp1$ and $Sn2$ switch assemblies, connected to the negative terminal of $C2$ capacitor, $Ref2$.

C. Design Considerations for the Bipolar Marx Generator

For the objective described in this application, the bipolar generator circuit in Fig. 3 was assembled with ten stages, 11 capacitors, for an U_{dc} up to about 850 V. For the Sp_i and Sn_i switches TO-263-7 C3M0065100J SiC Cree MOSFETs (i.e., 1000-V, 90-A pulsed current, and 65 m Ω) were chosen. Considering the pulse current and voltage hold-off, a series of two parallel devices was assembled as switches Sp_i and Sn_i , using four MOSFETs $S1$ – $S4$, as shown in Fig. 5.

Considering $R_{ai} = R_{bi} = 50 \Omega$, then the total switch Sp_i and Sn_i current is 194 A, as (2), meaning that each MOSFET conduct a current of 97 A during pulse. Current sharing between the parallel MOSFETs is ensured by the trigger synchronization, equal track design and similar device characteristics. In order to improve the MOSFET series

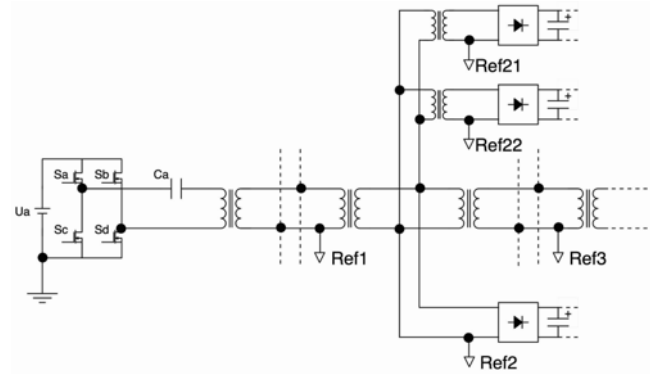


Fig. 6. Schematic simplified circuit for supplying power to each triggering stage, with details for the negative terminal of $C2$ capacitor, $Ref2$.

voltage sharing, a $R_{ii} C_{ii}$ parallel branch was inserted, also, with 1 M Ω and 1 nF, as shown in Fig. 5.

The value 16 μ F was chosen for the C_i capacitance, comprising eight parallel 2- μ F B32774D0205K0 EPCOS capacitors, giving 57.8-J stored energy in the Marx, and 96.8 ms to charge C_{11} , as (1). Even after considering the increase of the pulse current, by the self-discharge capacitor's current i_{Rai} and i_{Rbi} , the estimated pulse voltage droop is less than 40 V, lower than the ± 80 -V limit for the pulse flat top.

The pulse trigger signal is sent by fiber optics to the MOSFET drivers, where optical receiver HFBR-2521Z, optical transmitter HFBR-1521Z, and optical cable HFBR-RUS100Z, were used.

The signals from the fiber optics need to be amplified to fire the switches. Hence, in order to supply the power to all the switch drivers in the stages, a string of toroidal transformer was implemented, which is fed by a 100-kHz inverter, as shown in Fig. 6.

As seen in Fig. 6, $Ref1$ is associated with the negative terminal of $C1$, $Ref2$ is associated with the negative terminal of $C2$ (i.e., switches $S1$ and $S4$ from $Sp1$ and switches $S1$ and $S4$ from $Sn2$), shown in Fig. 5, and so on. In addition, it is shown, in Fig. 5, the supply of power for the electronics located in $Ref21$ (i.e., switches $S2$ and $S3$ from $Sp1$) and $Ref22$ (i.e., switches $S2$ and $S3$ from $Sn2$), as seen in Fig. 5. In summary, there is a primary transformer string for each Marx stage for supplying power to the electronics in Ref_i , and from that two more additional transformers are used to power different voltage references, Ref_{ji} .

III. RESULTS AND ANALYSIS

The implemented Marx generator is shown in Fig. 7, which is enclosed in a grounded 19" stainless steel box, without any ventilation apertures to minimize electromagnetic interference and the input of dust from outside as well.

In Fig. 7, the implemented Marx generator can be divided in two parts, the left and right, respectively, for the positive and negative pulse circuits, which are triggered by side position optic fibers. In between the positive and negative stacks, there are toroidal transformers that supply power to the triggering stages, as described in Fig. 6.

An experimental setup was assembled to test the generator, using an equivalent dummy load to the Kicker magnet, shown



Fig. 7. Top view picture of the 19-inch rack of the generator. A: Marx generator, B: control μ C board, and C: auxiliary power supplies and safety interlocks.

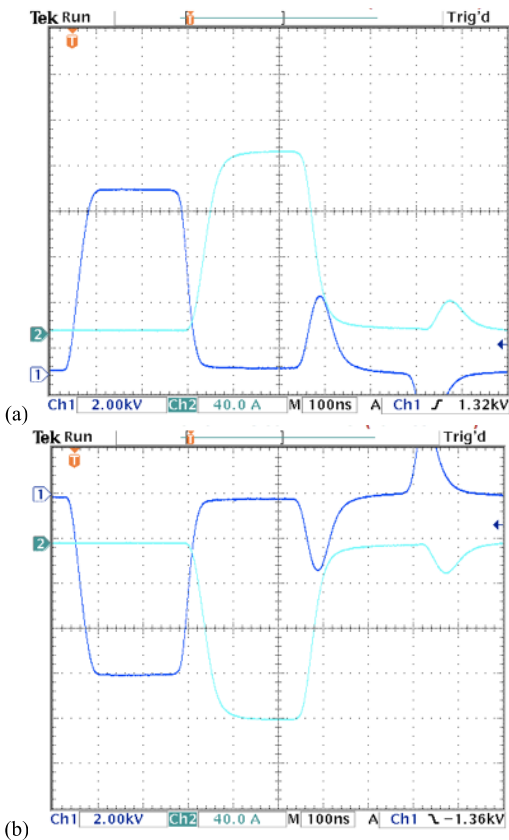


Fig. 8. Output Marx generator voltage (blue) and load current (cyan). (a) Positive pulse. (b) Negative pulse. Voltage 2 kV/div, current 40 A/div, and 100 ns/div.

in Fig. 1, comprising a $50\text{-}\Omega$ noninductive resistor in series with a piece of copper wound to give $1.2\text{-}\mu\text{H}$ load, connected to the generator by HV RG 218 50-m cable. Unless described

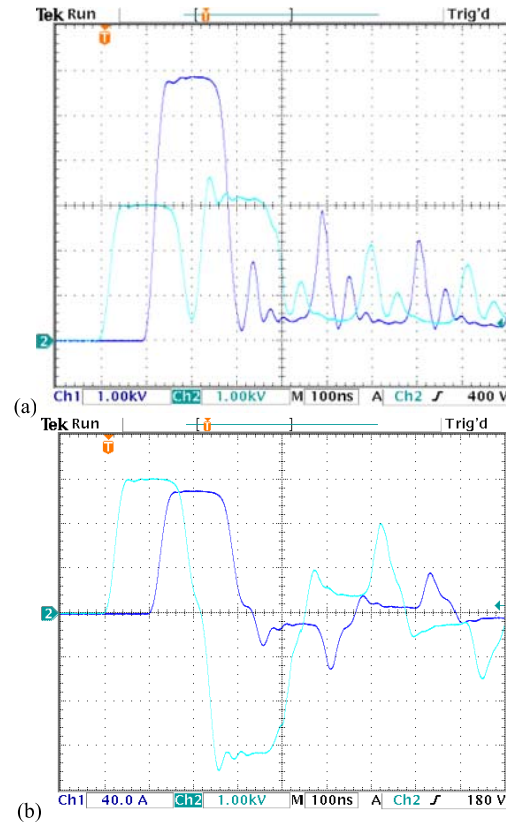


Fig. 9. (a) Open-load condition, output Marx generator voltage (cyan) and open-end cable voltage (blue). (b) Load short-circuit condition, output generator voltage (cyan) and short-circuit load current (blue): 1 kV/div, current 40 A/div, and 100 ns/div.

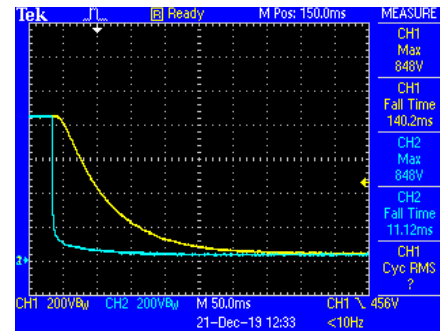


Fig. 10. Discharge of C1 (cyan) and C11 (yellow) capacitors, with full charged Marx, during an emergency: 50 ms/div and 200 V/div.

otherwise, voltage waveforms were recorded with a Tektronix TPS2024B 200-MHz 2-GS/s oscilloscope, using PMK PHV1000 100:1 400-MHz $50\text{-M}\Omega/7.5\text{-pF}$ high voltage probe. The current measurements were recorded using a Bergoz CT-E0.1-B current transformer.

A. Positive and Negative Pulse Operation

Fig. 8 shows the output Marx generator 8-kV positive and negative, 350-ns width, voltage pulses and 160-A load currents, considering an 850-V external input voltage.

It can be seen, from Fig. 8, that the voltage reflection at about 500 ns is compatible with the length of the cable used for testing, i.e., 50 m, and the 5 ns per meter propagation velocity. Also, it is seen in Fig. 8, the load current shifted by 250 ns, from the Marx pulse voltage output. In addition,

the risetime and falltime for the current pulses are about 57 ns, between 10% and 90%.

B. Open-Circuit and Short-Circuit Operation

Fig. 9 shows the operation of the Marx generator for two fault conditions: (1) load not connected, cable end open-circuit and (2) load short-circuit, cable end short-circuit. These results were taken for a 20-m cable length connection, considering a 300-V external input voltage.

It can be seen, from Fig. 9(a), for the open-circuit condition (i.e., transmission coefficient of 2 and reflection coefficient of 1), the voltage at the open-cable end with twice the output Marx voltage and the output Marx voltage with a reflection after 200 ns, corresponding to the 20-m cable. In addition, it can be seen, from Fig. 9(b), for the short-circuit condition (i.e., transmission coefficient of 0 and reflection coefficient of -1), the short-circuit current at the load shifted 100 ns from the output Marx voltage, and negative output Marx voltage reflection after 200 ns, corresponding to the 20-m cable.

Finally, Fig. 10 shows the discharge of the C1 and C11 capacitors, during an emergency situation (e.g., vacuum fault), where the switch in parallel with C1 capacitor is turned ON. As seen, the time constant of the discharge increases from the first C1 to the last C11, nevertheless the last capacitor achieves a voltage of 50 V in less than 300 ms, within the safety regulations.

IV. CONCLUSION

A bipolar Marx generator, based on SiC MOSFETs, was demonstrated to deliver bipolar pulses to a dummy load, equivalent of the Berlin BESSY II injection kicker, with the following pulse specifications: (1) peak voltage of ± 8 kV, (2) peak current of 160 A, (3) impedance of 50 Ω , (4) frequency ≤ 10 Hz, (5) width of 350 ns, (6) risetime ≤ 80 ns, and (7) deviation from "Flat top" $\leq \pm 1\%$. In addition, the circuit path to charge the Marx capacitors is based on resistors which allow both for the charge of the capacitors within 100 ms and the fast discharge of the Marx energy in less than 300 ms in case of an emergency.

Plans for future include a more detailed analysis of generator operation using the real Kicker injection system.

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